

# Modelling Multiphase and Interfacial Flows with Complex Geometries using LBM

**Prof Halim Kusumaatmaja**

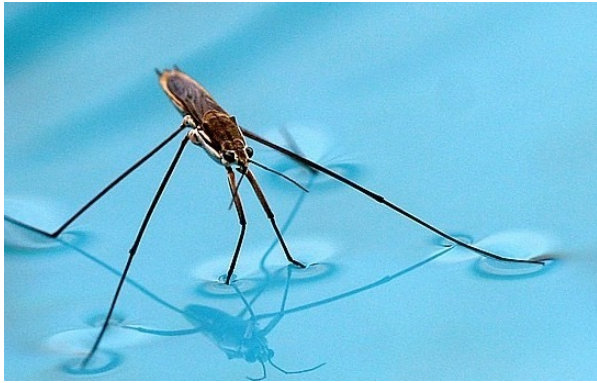
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Institut Henri Poincaré

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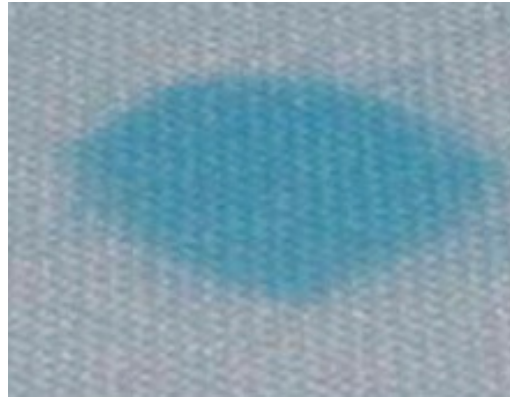
# Wetting Phenomena as Underpinning Science

## Biology



*Water Strider*

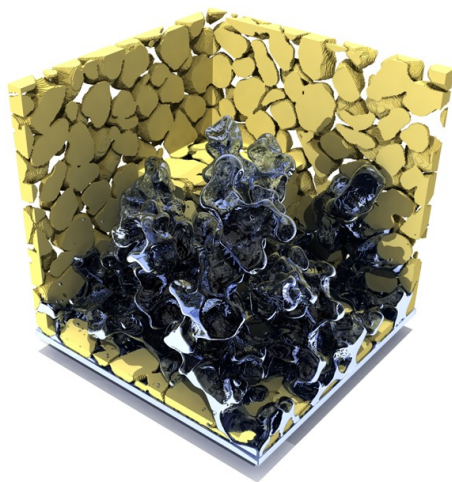
## Fabrics



## Electronics



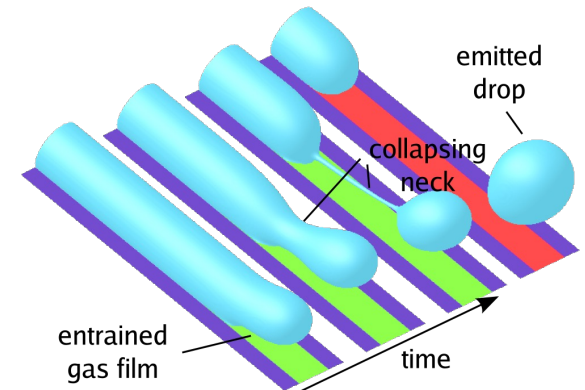
## Oil Recovery



## Paints & Coatings



## Microfluidics



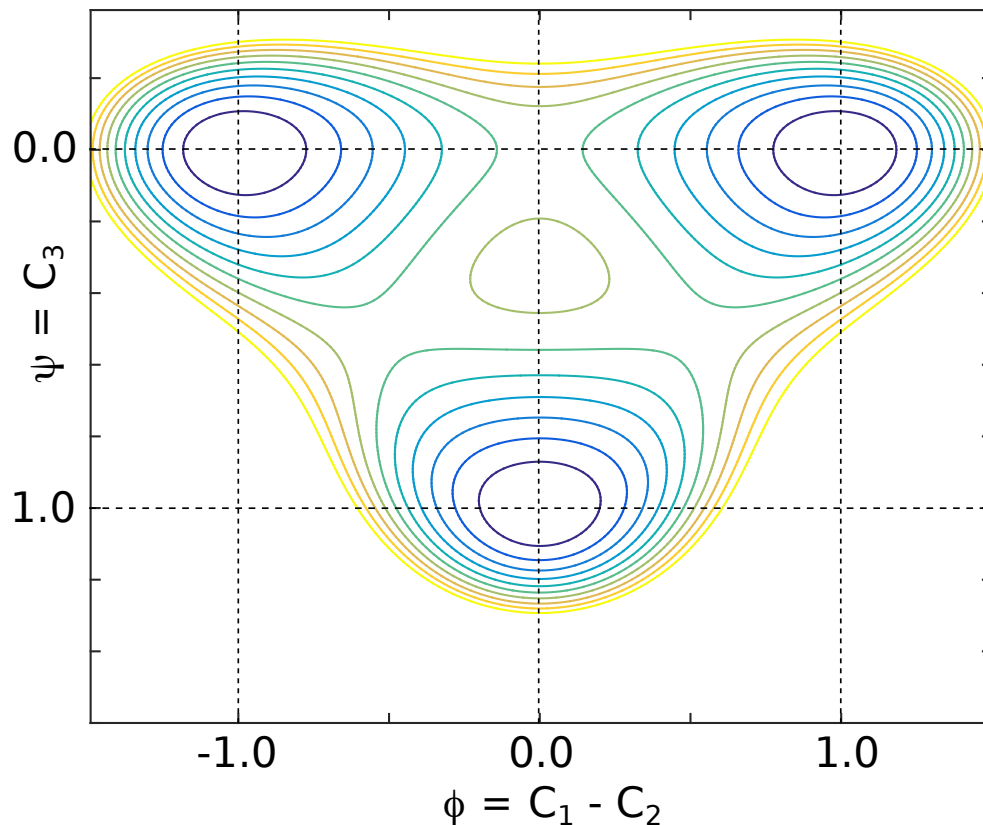
# Ternary Fluid Flows

# Free Energy LBM

**Free energy** (similar to diffuse interface / phase field model)

$$F = \int_{\Omega} \left[ \frac{\kappa_1}{2} C_1^2 (1 - C_1)^2 + \frac{\kappa_2}{2} C_2^2 (1 - C_2)^2 + \frac{\kappa_3}{2} C_3^2 (1 - C_3)^2 \right] dV \quad \leftarrow \text{Double wells}$$
$$+ \int_{\Omega} \left[ \frac{\alpha^2 \kappa_1}{2} (\vec{\nabla} C_1)^2 + \frac{\alpha^2 \kappa_2}{2} (\vec{\nabla} C_2)^2 + \frac{\alpha^2 \kappa_3}{2} (\vec{\nabla} C_3)^2 \right] dV \quad \leftarrow \text{Gradients}$$

e.g. Semperebon, Krüger, **HK**, PRE (2016); Boyer & Lapuerta, ESAIM (2006)



Given constraint  $C_1 + C_2 + C_3 = 1$

**Three independent energy minima**

$$C_1 = 1, \quad C_2 = 0, \quad C_3 = 0;$$

$$C_1 = 0, \quad C_2 = 1, \quad C_3 = 0;$$

$$C_1 = 0, \quad C_2 = 0, \quad C_3 = 1.$$

Interface width  $\alpha$

$$\text{Surface tension} \quad \gamma_{mn} = \frac{\alpha}{6} (\kappa_m + \kappa_n)$$

# Equations of Motion – Numerical Scheme

The **macroscopic equations** we solve are:

- Continuity equation

$$\partial_t \rho + \partial_\alpha (\rho u_\alpha) = 0$$

- Navier-Stokes equation

$$\partial_t (\rho u_\alpha) + \partial_\beta (\rho u_\alpha u_\beta) = -\partial_\beta P_{\alpha\beta} + \partial_\beta \eta (\partial_\beta u_\alpha + \partial_\alpha u_\beta) + F_\alpha$$

MRT scheme with Guo forcing / Exact Difference Method

- Cahn-Hilliard equation

Chemical force  $F_\alpha = -\phi \partial_\alpha \mu_\phi$

$$\partial_t \phi + \partial_\alpha (\phi u_\alpha) = M_\phi \nabla^2 \phi$$

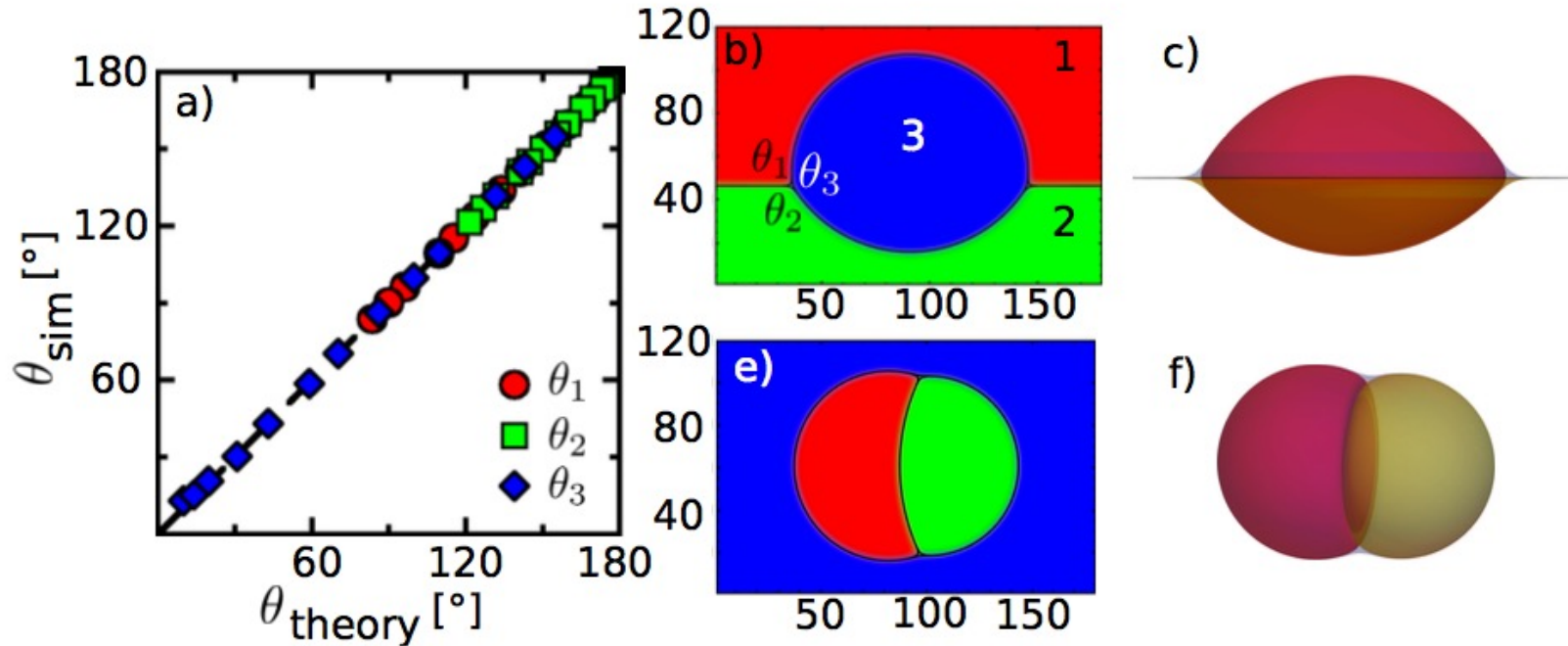
BGK scheme

Chemical potential  $\mu_\phi = \frac{\delta F}{\delta \phi}$

Need more than one Cahn-Hilliard equation if we have > 2 components

# Neumann Triangle

Semprebon, Krüger, **HK**, PRE (2016)



Balance of surface tension

$$\Rightarrow \vec{\gamma}_{12} + \vec{\gamma}_{23} + \vec{\gamma}_{31} = 0$$

$$\Rightarrow \frac{\gamma_{23}}{\sin \theta_1} = \frac{\gamma_{31}}{\sin \theta_2} = \frac{\gamma_{12}}{\sin \theta_3}$$

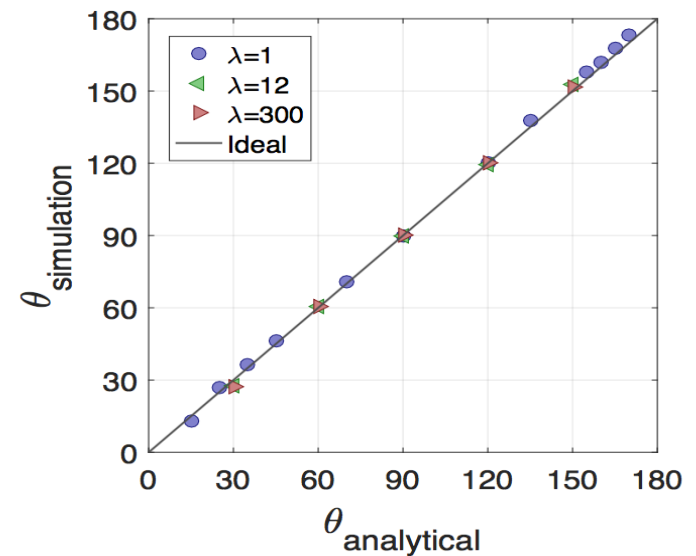
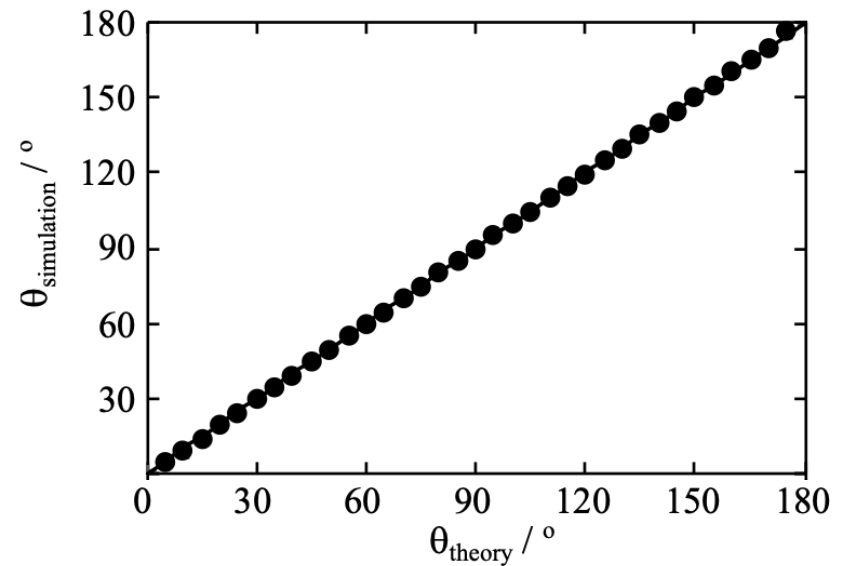
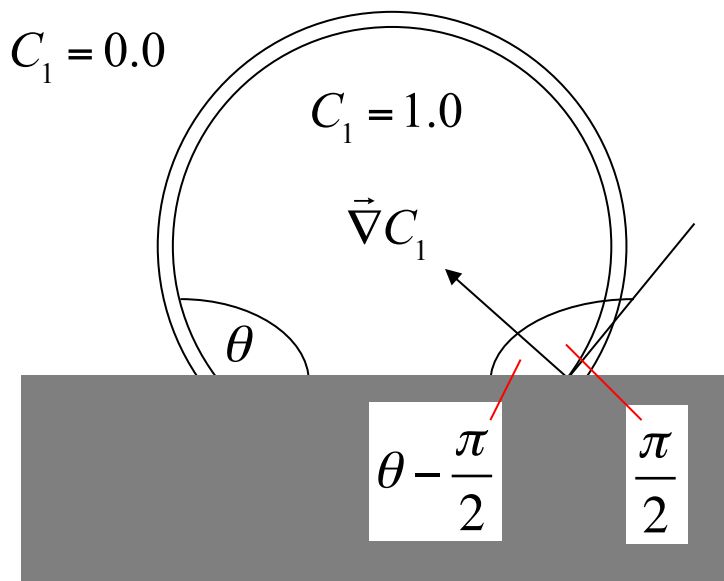
# Implementing Contact Angles

## Cubic Wetting Boundary Condition

$$\mathbf{n} \cdot \nabla C_m|_S = \sum_{m=1}^N \xi_{mn} C_m C_n$$

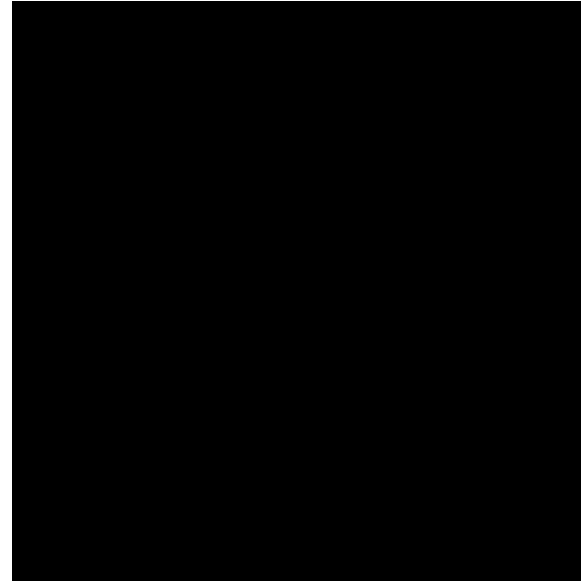
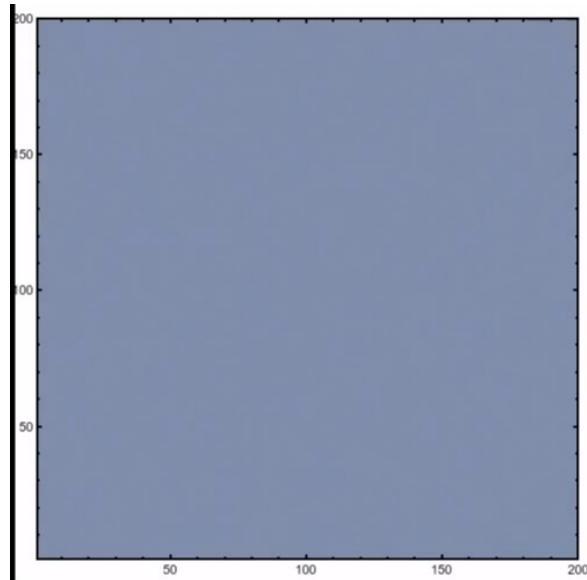
$$\xi_{mn} = \frac{4}{\varepsilon} \cos \theta_{mn}$$

## Geometric boundary condition:



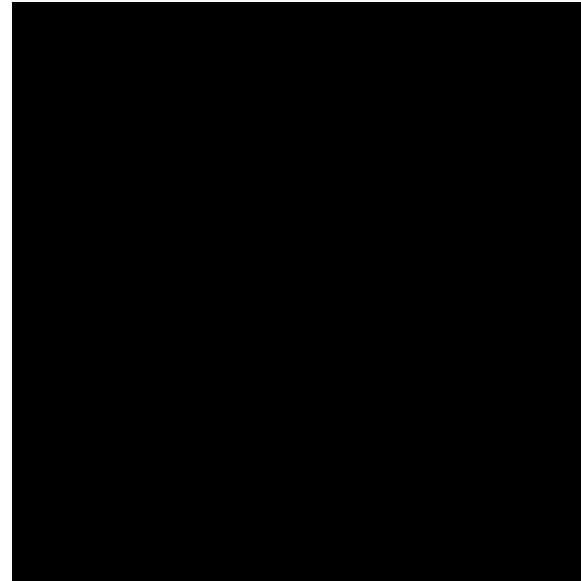
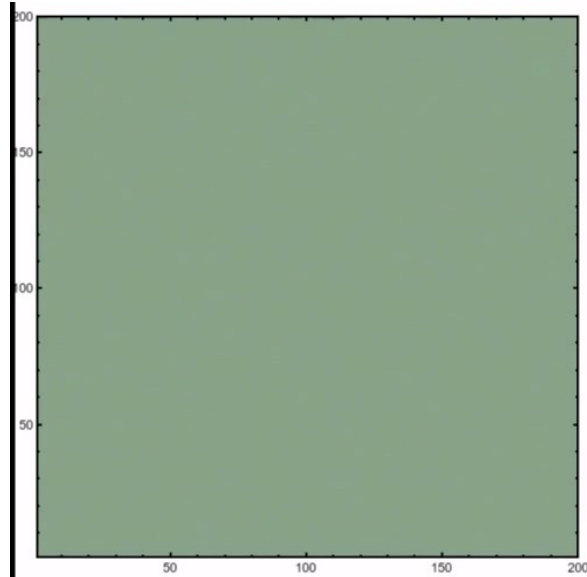
# Example: Phase Separation

$$c_1 = c_2 = c_3$$



$$c_1 = c_2$$
$$c_1 + c_2 < c_3$$

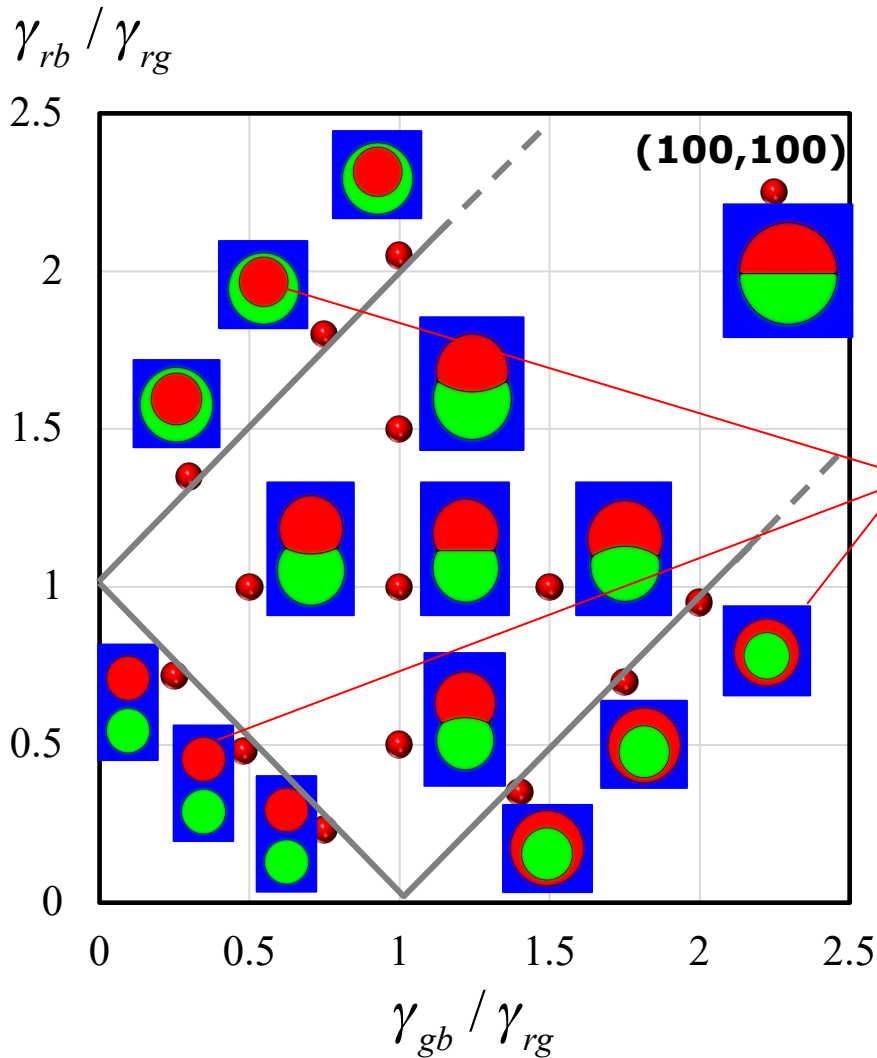
$$c_1 = c_2 \gg c_3$$



$$c_1 = c_2$$
$$c_1 + c_2 > c_3$$



# Problem: Droplet Cloaking



## Free energy

$$F = \int_{\Omega} \left[ \frac{\kappa_1}{2} C_1^2 (1 - C_1)^2 + \frac{\kappa_2}{2} C_2^2 (1 - C_2)^2 + \frac{\kappa_3}{2} C_3^2 (1 - C_3)^2 \right] dV$$

$$+ \int_{\Omega} \left[ \frac{\alpha^2 \kappa_1}{2} (\vec{\nabla} C_1)^2 + \frac{\alpha^2 \kappa_2}{2} (\vec{\nabla} C_2)^2 + \frac{\alpha^2 \kappa_3}{2} (\vec{\nabla} C_3)^2 \right] dV$$

Surface tension  $\gamma_{mn} = \frac{\alpha}{6} (\kappa_m + \kappa_n)$

Requires negative values of kappa's.

## Example:

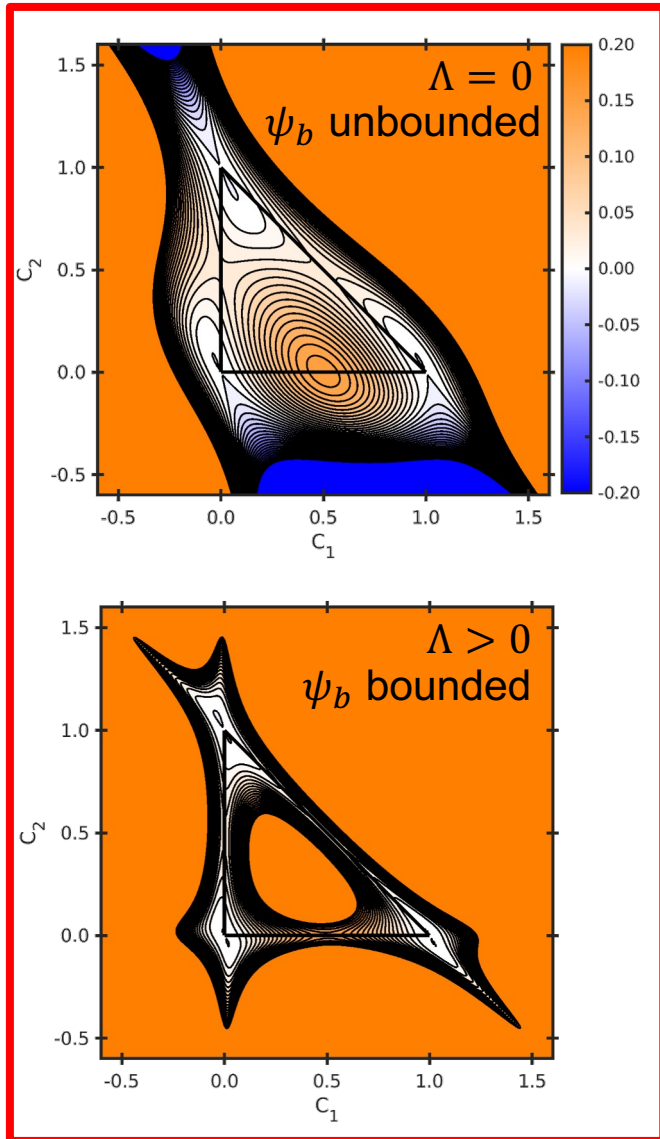
$$\gamma_{rb} + \gamma_{gb} < \gamma_{rg}$$

$$(\kappa_r + \kappa_b) + (\kappa_g + \kappa_b) < (\kappa_r + \kappa_g)$$

$$2\kappa_b < 0$$

The double well potential is unbounded

# Problem: Droplet Cloaking



## Free energy

$$F = \int_{\Omega} \left[ \frac{\kappa_1}{2} C_1^2 (1 - C_1)^2 + \frac{\kappa_2}{2} C_2^2 (1 - C_2)^2 + \frac{\kappa_3}{2} C_3^2 (1 - C_3)^2 \right] dV$$
$$+ \int_{\Omega} \left[ \frac{\alpha^2 \kappa_1}{2} (\vec{\nabla} C_1)^2 + \frac{\alpha^2 \kappa_2}{2} (\vec{\nabla} C_2)^2 + \frac{\alpha^2 \kappa_3}{2} (\vec{\nabla} C_3)^2 \right] dV$$

$$\text{Surface tension} \quad \gamma_{mn} = \frac{\alpha}{6} (\kappa_m + \kappa_n)$$

Requires negative values of kappa's.

Need to add "penalty term"

$$\Delta F_b = \Lambda C_1^2 C_2^2 C_3^2$$

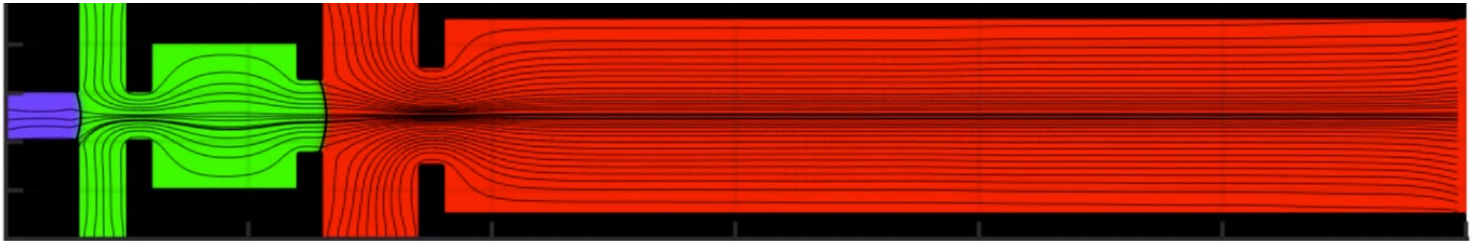
# Example: Droplet Microfluidics

- Wang et al., J. Fluid Mech. 895, A22 (2020)

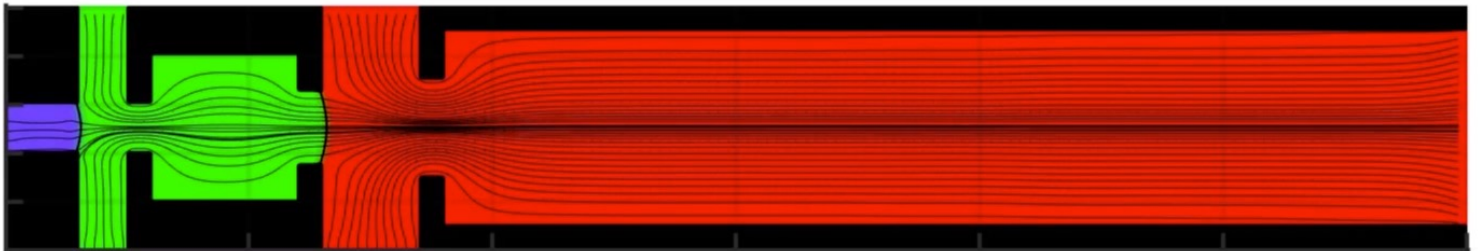
**Full  
Wetting**



**Neutral  
Wetting**



**Non  
Wetting**



# Example: Liquid Infused Surfaces

**Dry**

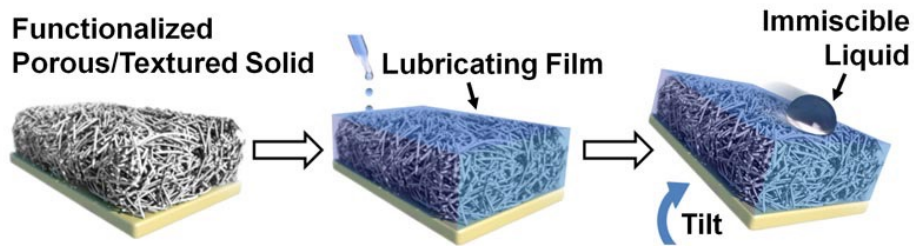


**Wet**

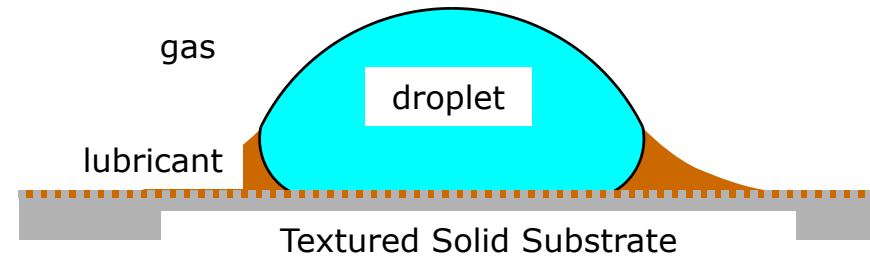


Youtube

## Preparation



## Typical Geometry Considered



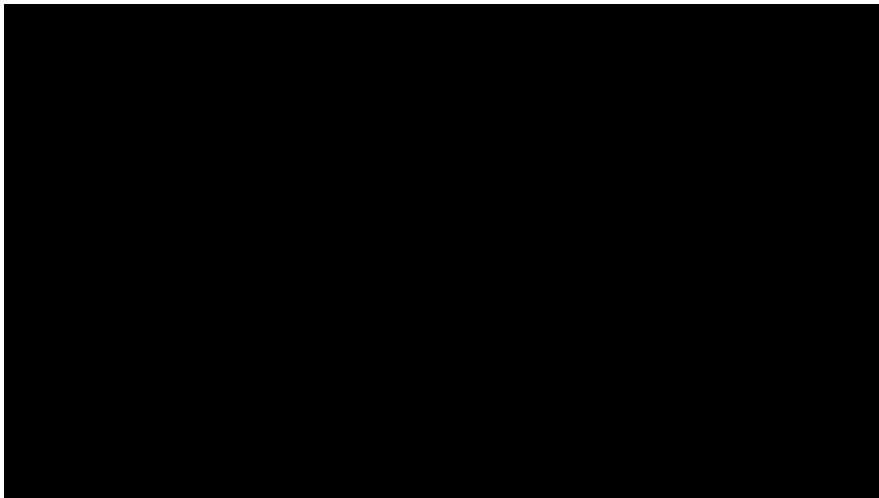
Wong et al., Nature (2011); Lafuma & Quere, Europhys. Lett. (2011); and many others...

# Applications of LIS

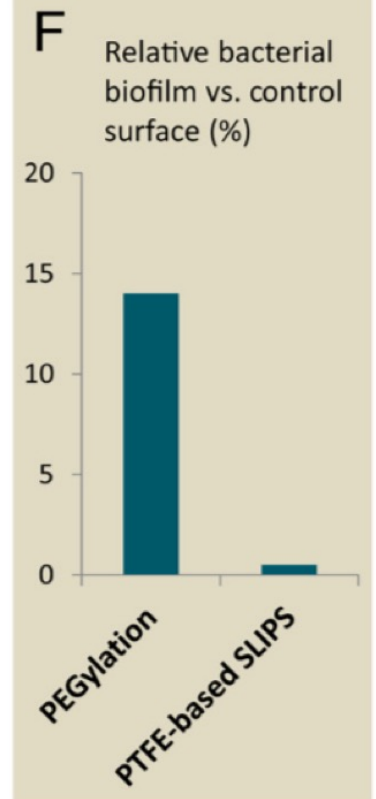
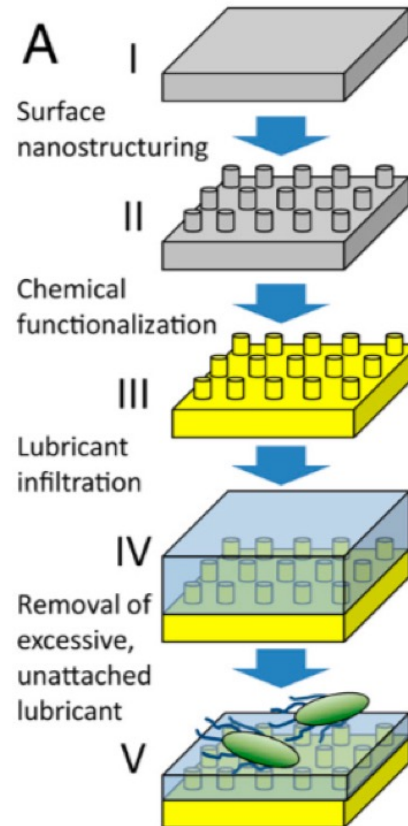
## Packaging



## Paint



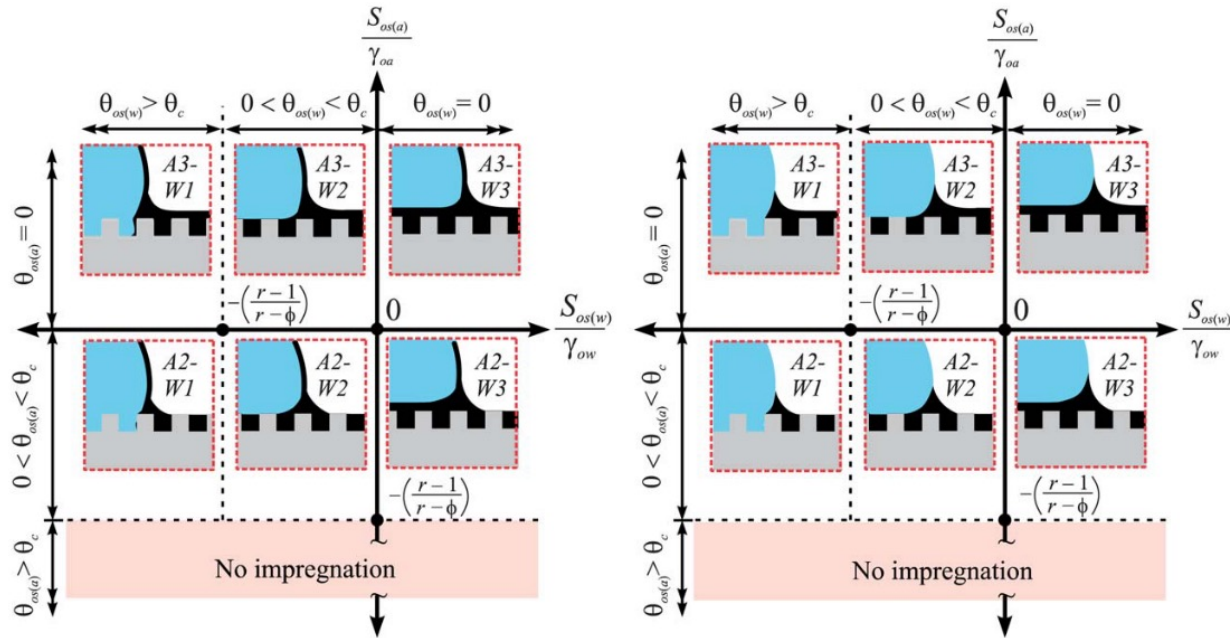
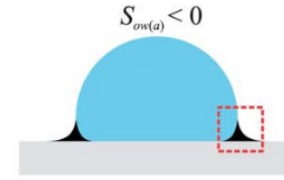
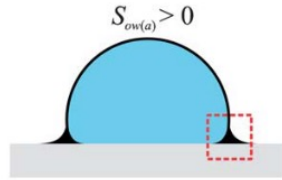
## Anti Biofouling



# Possible Wetting States

## Thermodynamic Model:

Smith et al., Soft Matter (2013)



Spreading Coefficient:

$$S_{ij(k)} = \gamma_{jk} - \gamma_{ij} - \gamma_{ik}$$



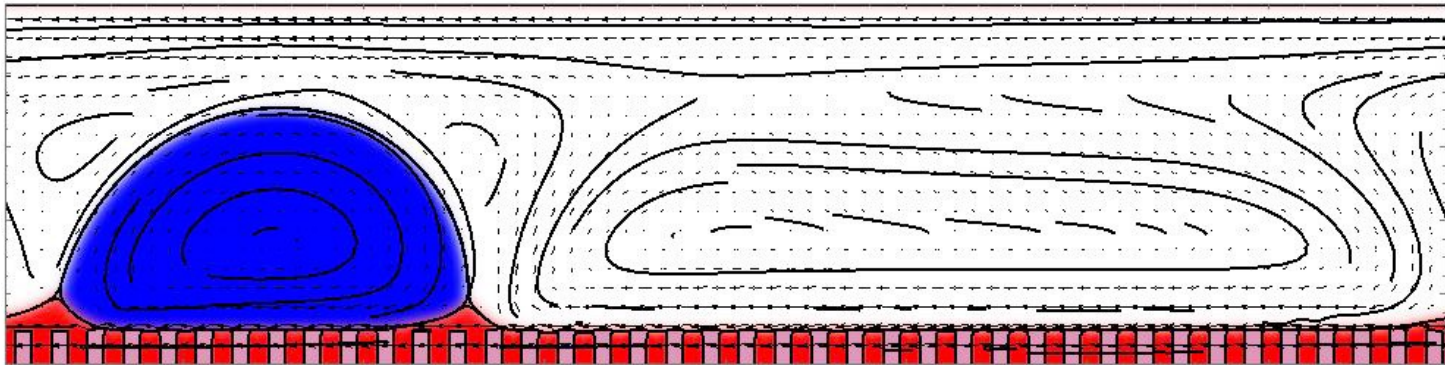
If  $S_{ij(k)} > 0$ , cloaking takes place.

$$\gamma_{jk} > \gamma_{ij} + \gamma_{ik}$$

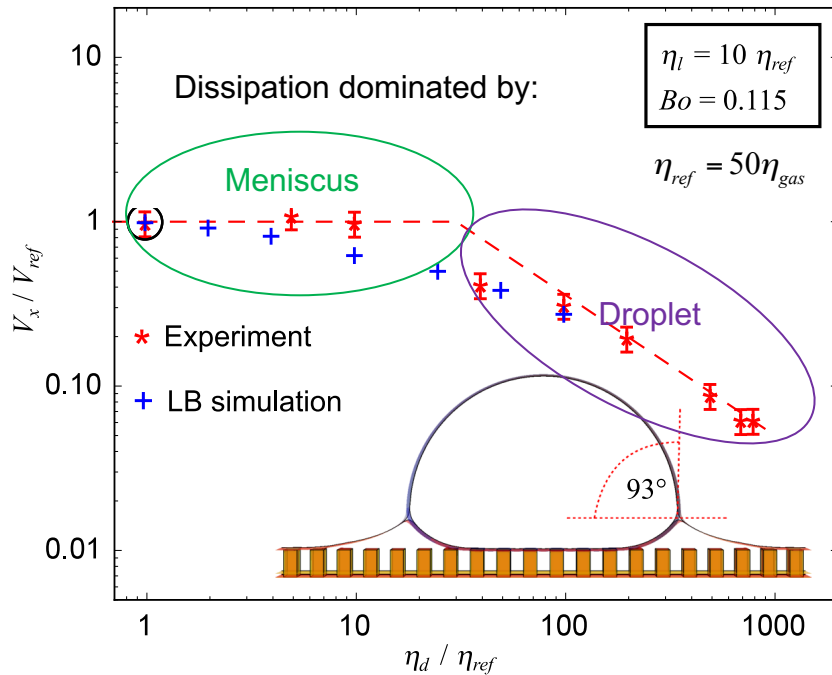
$jk$  interface is unfavourable.

# Drop Dynamics

□ Sadullah et al., Langmuir 34, 8112 (2018); Naga et al., in preparation (2023)

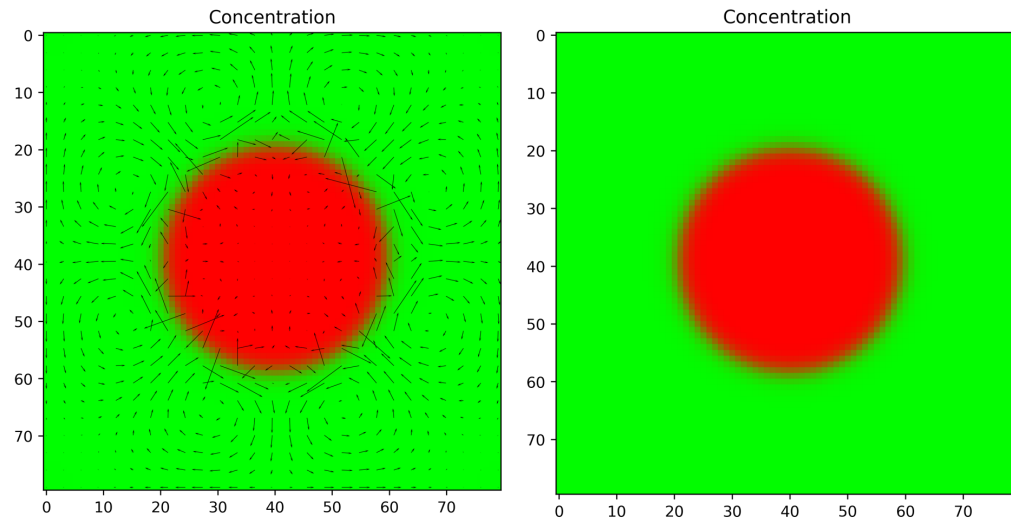


Experimental data: Keiser et al., Soft Matter (2017)



But can we look into the dissipation profile?

Problems with Spurious Velocities



Max velocity  $\sim 10^{-5}$

Max velocity  $\sim 10^{-15}$

Scheme from T. Lee and L. Liu, J. Comput. Phys. (2010)

# Incompressible Multiphase Scheme

**Key Scheme:** Use approach proposed by Lee and Liu, JCP 2010

- Incompressible 2-component flow: Boltzmann equation for pressure and momentum
- Mixed stencils for the spatial gradients: Required for the macroscopic variables
- Wetting boundary conditions for the chemical potential and order parameters (concentrations)

**Extension to 3-component has been done**

- Similar to work by Abadi et al., PRE 97, 033312 (2018) and several others from this group
- 2-D and no solid boundaries

**Additional Extension Required**

- 3D using D3Q19
- Solid boundaries

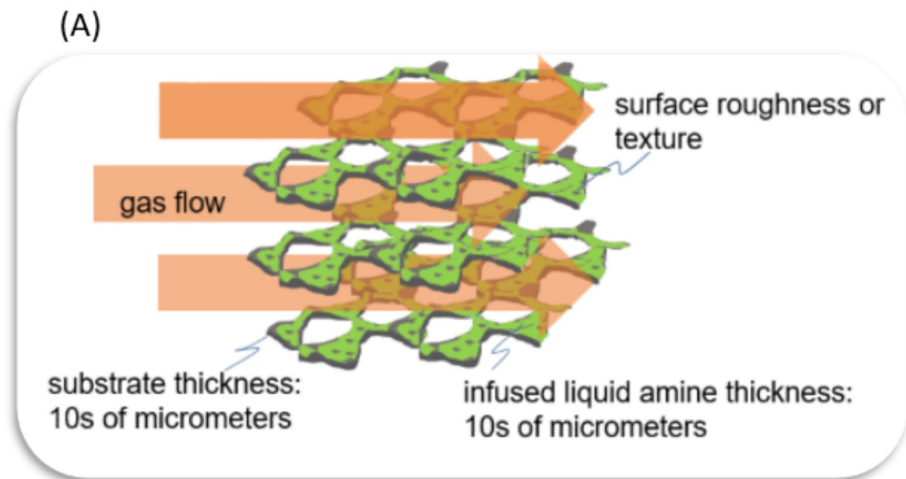


# Evaporation on Structured Surfaces

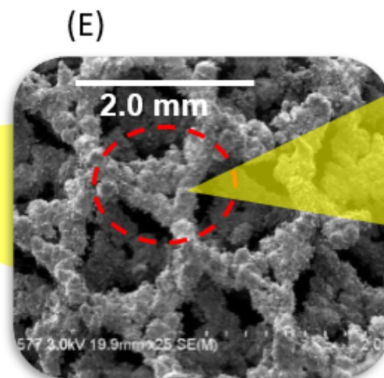
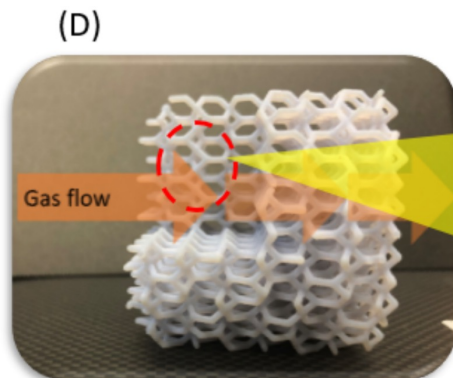
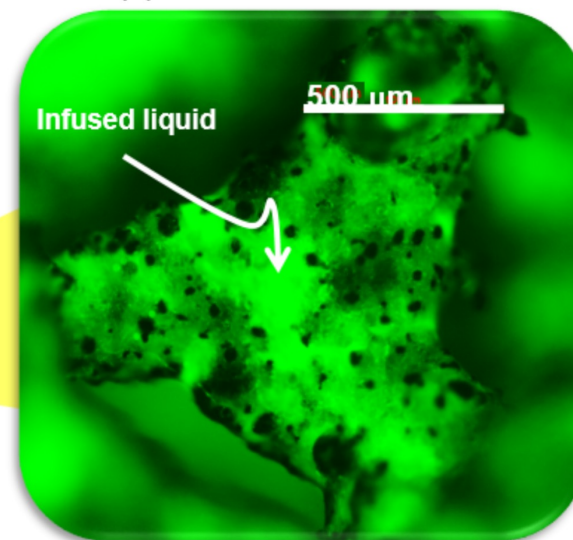
# Solid with Infused Reactive Liquid

□ M. S. Yeganeh et al., Science Advances (2022)

**Application:** carbon capture



(F)



**ExxonMobil**

# Model

## Continuity & Navier Stokes

$$\frac{\partial}{\partial t}(\rho) + \nabla \cdot (\rho \mathbf{u}) = 0$$

$$\frac{\partial(\rho \mathbf{u})}{\partial t} + \nabla \cdot (\rho \mathbf{u} \mathbf{u}) = -\nabla p + \nabla \cdot [\mu(\nabla \mathbf{u} + \nabla \mathbf{u}^T)] + \mathbf{F},$$

## Modified Cahn-Hilliard

$$\frac{\partial C}{\partial t} + \nabla \cdot (\mathbf{u}C) = \nabla \cdot (M \nabla \mu) \longrightarrow \frac{\partial C}{\partial t} + \nabla \cdot (\mathbf{u}C) = \nabla \cdot (M \nabla \mu) - \frac{\dot{m}'''}{\rho_l}$$

$$\dot{m}'' = \frac{\rho_{g,I} D}{1 - Y_v} \nabla Y_v \cdot \mathbf{n}. \quad \longrightarrow \quad \dot{m}''' = \frac{\rho_{g,I} D}{1 - Y_v} \nabla Y_v \cdot \nabla C$$

As source  
term

$$\frac{\dot{m}'''}{\rho_l}$$

Lee & Liu scheme,  
JCP (2010)

## Advection-Diffusion

$$\frac{\partial Y_v}{\partial t} + \mathbf{u} \cdot \nabla Y_v = \nabla \cdot (D \nabla Y_v).$$

BGK scheme

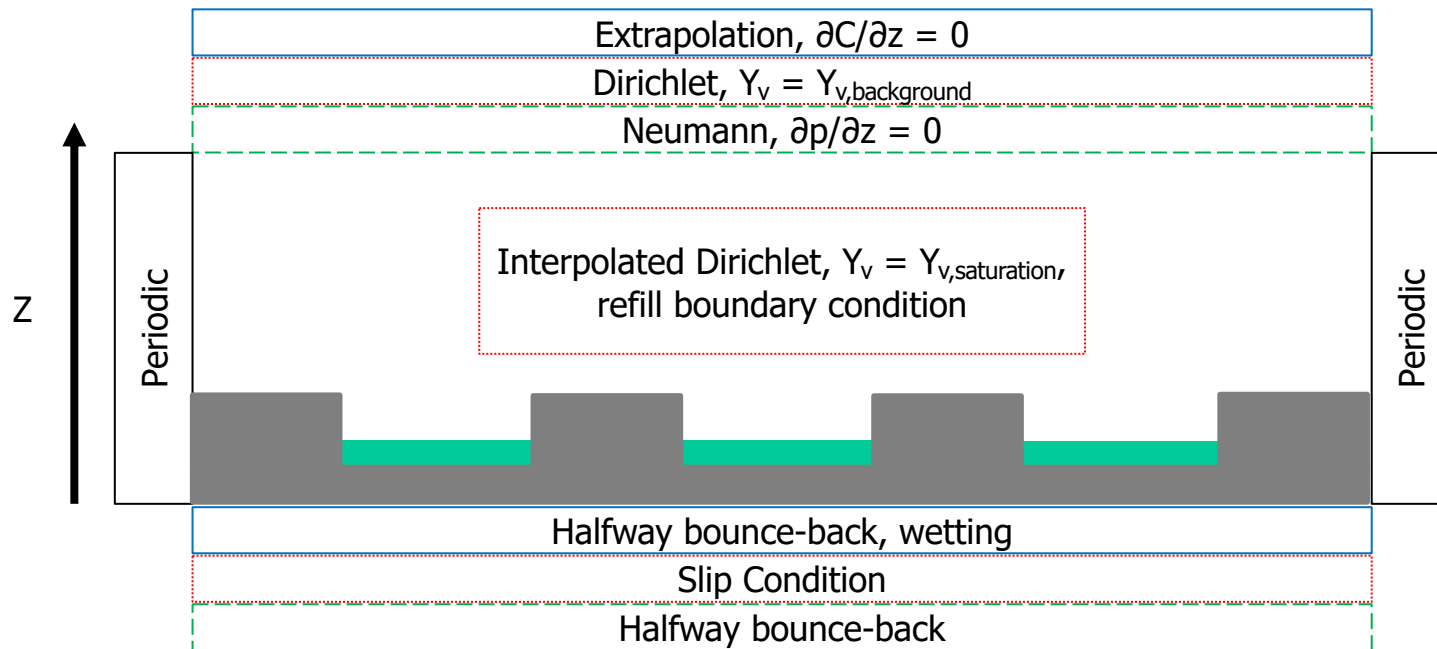
# Typical Simulation Setup

## Boundary Conditions

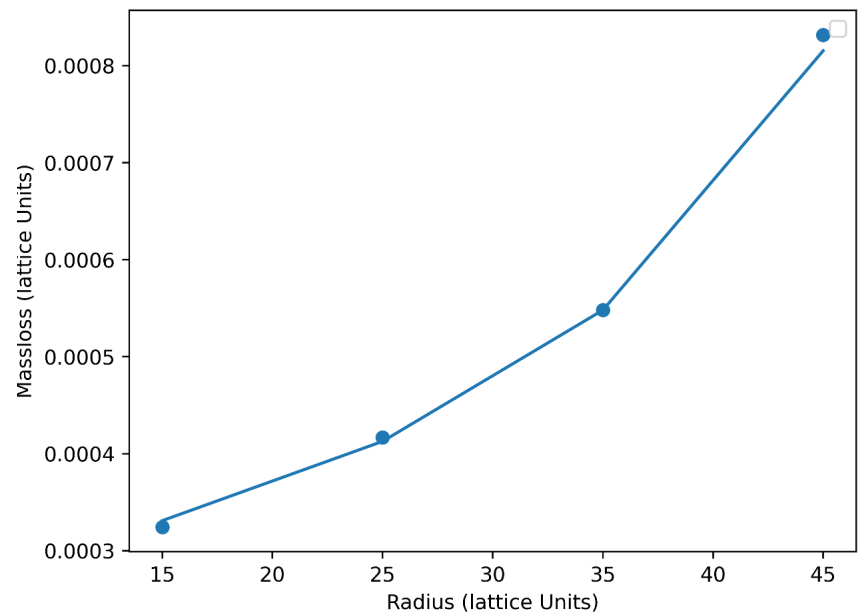
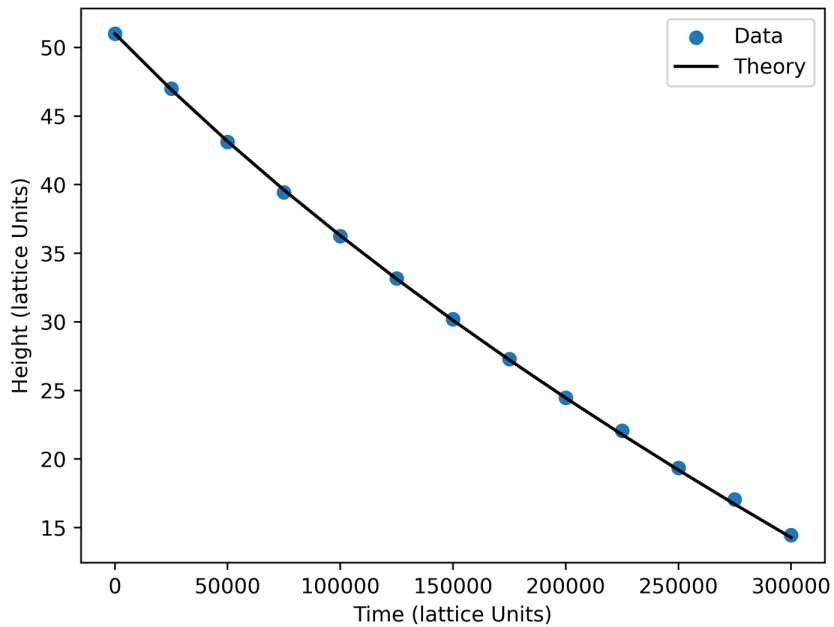
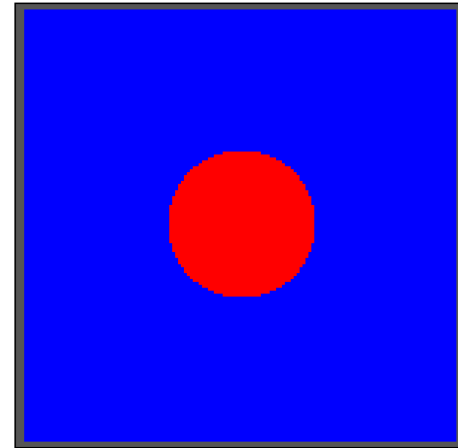
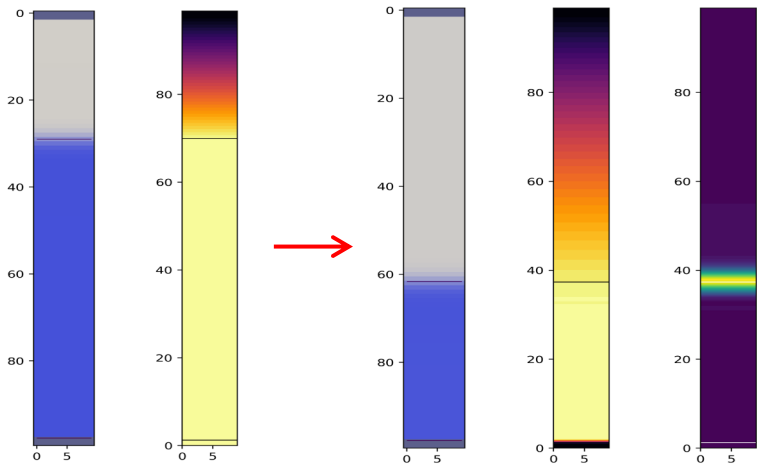
Navier Stokes

Advection-Diffusion for Vapor Concentration

Modified Cahn-Hilliard



# Benchmarks



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# Summary

- LBM is a powerful approach to study complex multiphase and interfacial flows
- Challenge I:  $N > 2$  components. We can capture accurate Neumann angles and Young's contact angles. Applications range from droplet microfluidics, liquid infused surfaces, and phase separation.
- Challenge II: Phase change phenomena (here, focussed on evaporation). We coupled multiphase LBM with humidity evolution. Multiphysics problems with complex boundary conditions.
- Challenge III: Complicated geometries. A different way to capture highly complex solid boundaries?

Thank you for listening!